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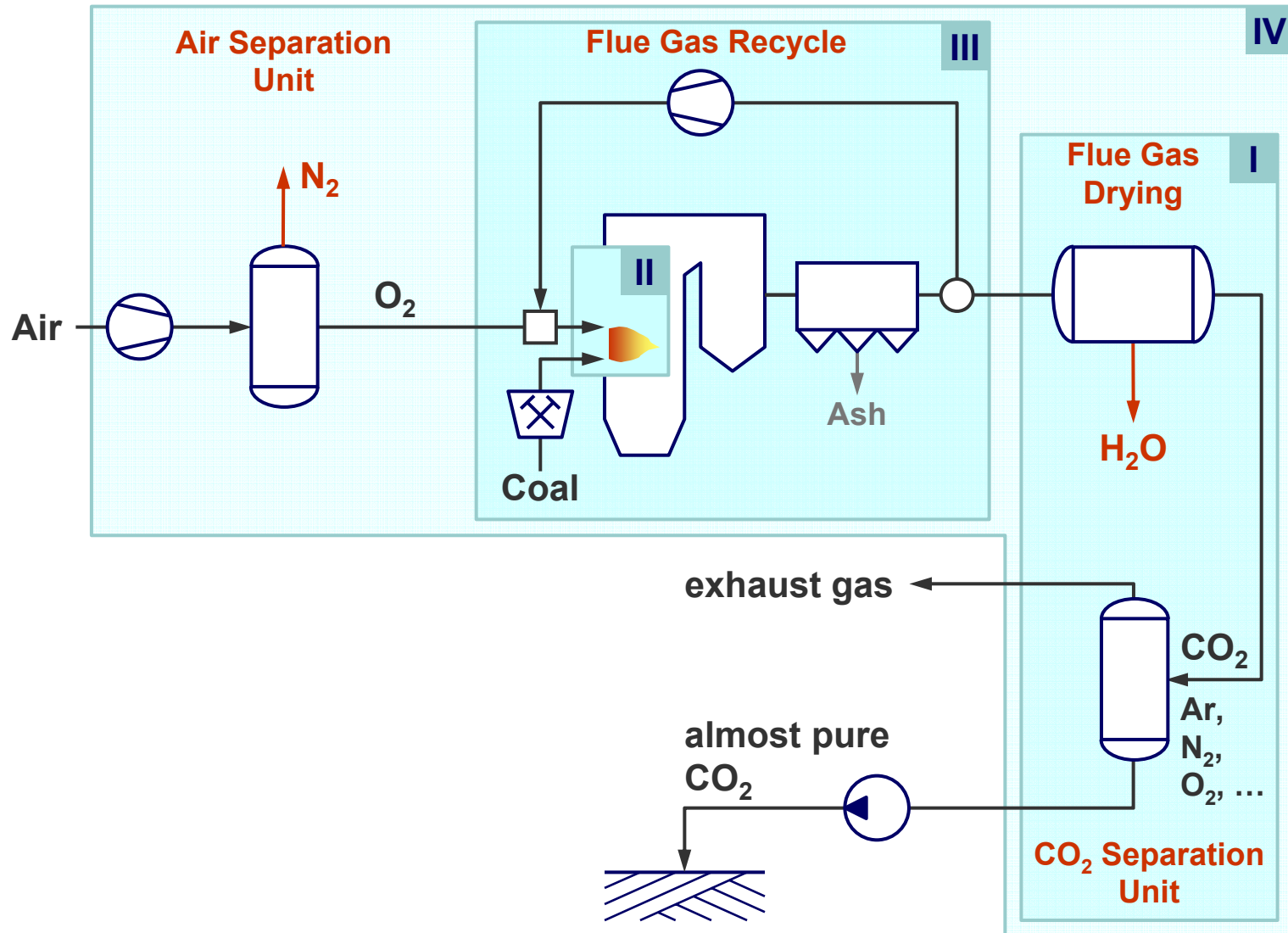
**Oxyfuel Process for Hard  
Coal with CO<sub>2</sub>-Capture**

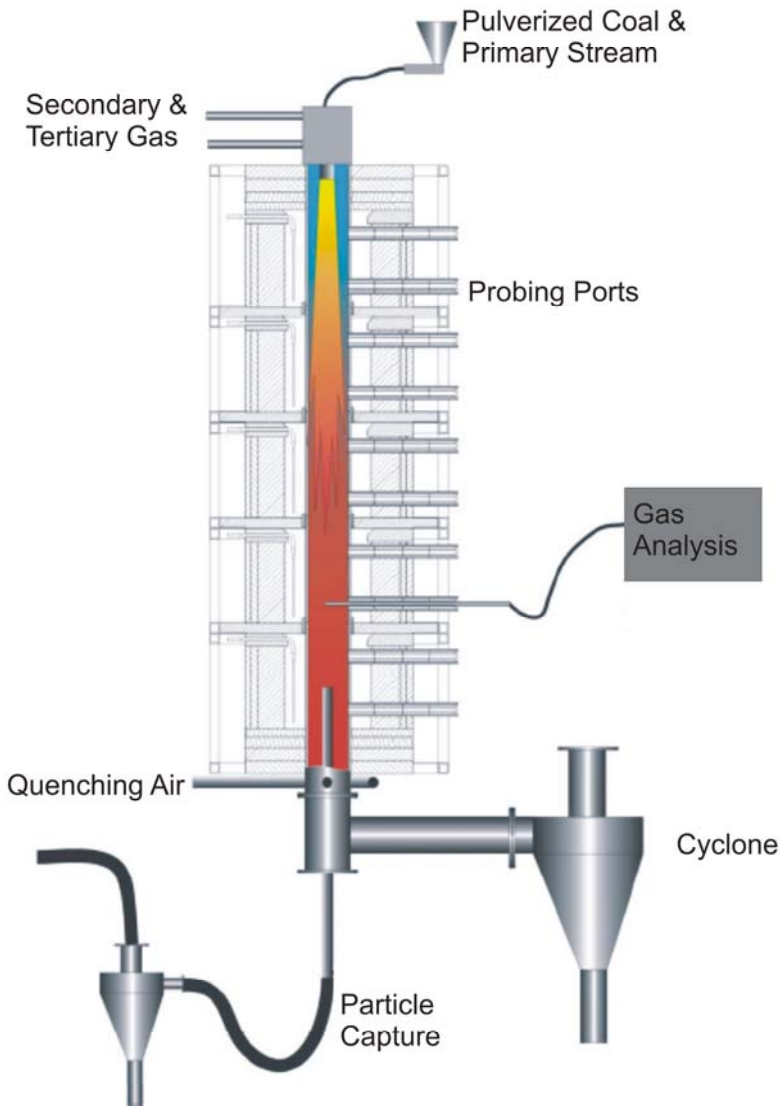
Current Research at TUHH

**TUHH**

*Technische Universität Hamburg-Harburg*

Young Researchers Meeting,  
December 8<sup>th</sup>, 2006, Hamburg





**Combustion capacity: 20 kW**

**Heated ceramic tube:**

**Ø150 mm, 2 m length,  
5 independent segments,  
900 – 1600 °C**

**Artificial combustion atmospheres  
by mixing O<sub>2</sub>, CO<sub>2</sub>, N<sub>2</sub>, NO, SO<sub>2</sub>,  
steam, and air**

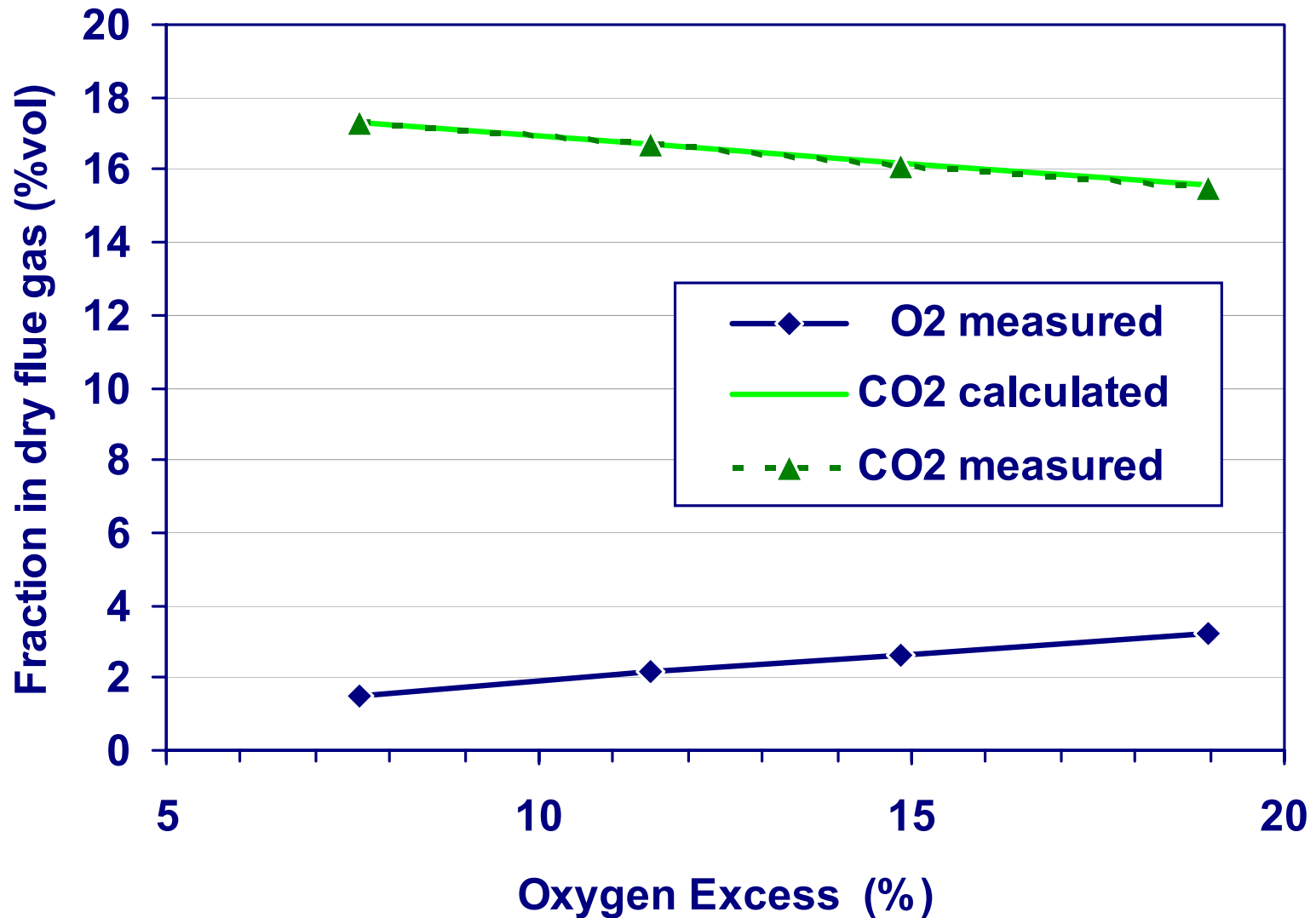
➔ **constant combustion conditions**

**Primary, secondary, tertiary stream and  
possibility of feed gas staging**

**Measurement of NO, NO<sub>2</sub>, CO, CO<sub>2</sub>, O<sub>2</sub>,  
SO<sub>2</sub>, and gas temperature**

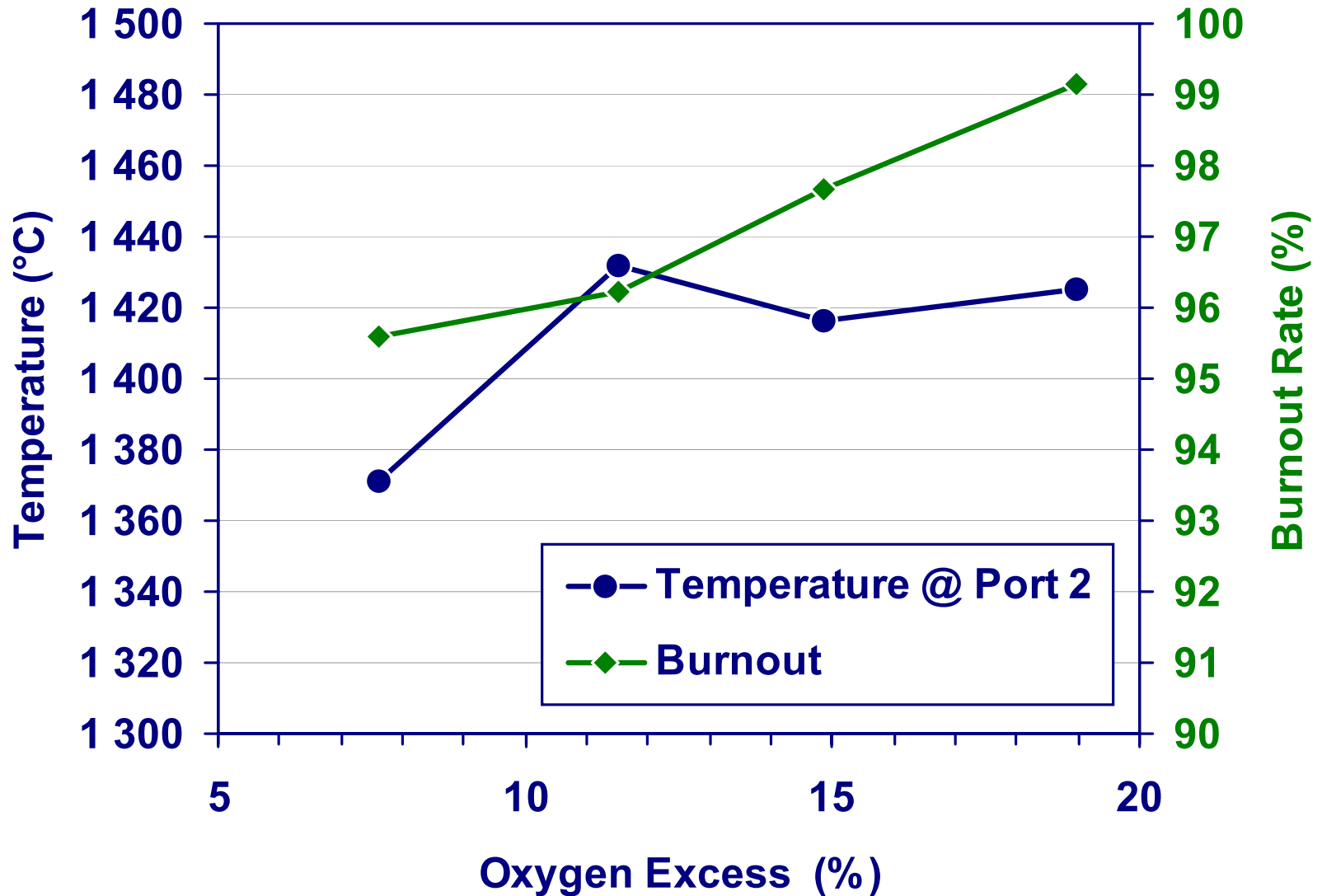
# Experimental Work

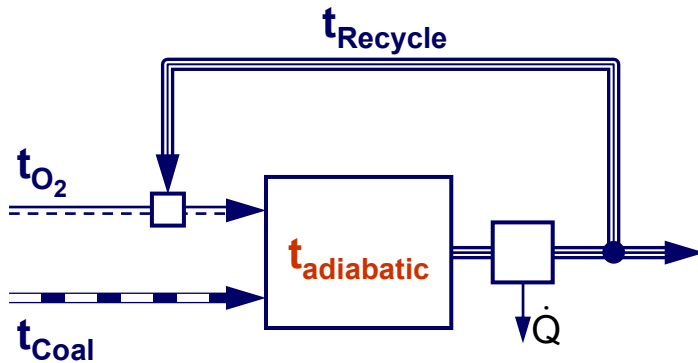
## Combustion of Indonesian Hard-Coal in Air



# Experimental Work

## Combustion of Indonesian Hard-Coal in Air





- Condition:

$$t_{\text{adiabatic w/ Air}} = t_{\text{adiabatic w/ O}_2 + \text{Recycle}}$$

- Underlying assumptions:

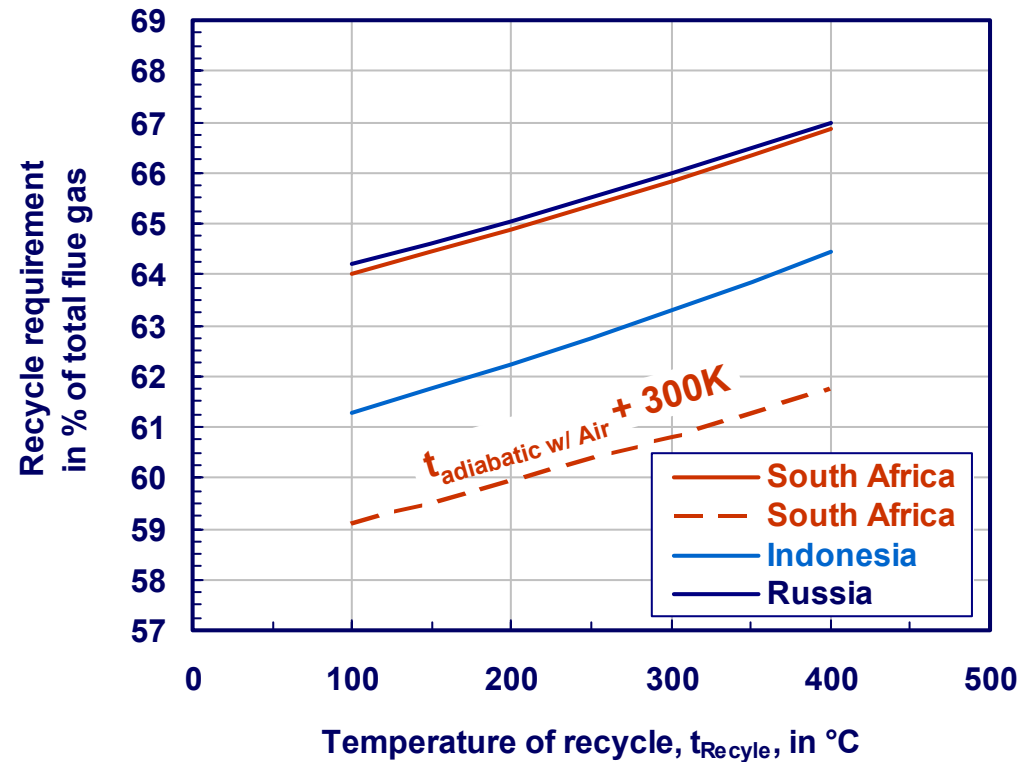
$$t_{\text{Air}} = 320 \text{ }^\circ\text{C}$$

$$t_{\text{O}_2} = 20 \text{ }^\circ\text{C}$$

$$t_{\text{Coal}} = 40 \text{ }^\circ\text{C}$$

$$\text{O}_2\text{-excess: } 15 \%$$

$$\text{O}_2\text{-purity: } 98 \%$$



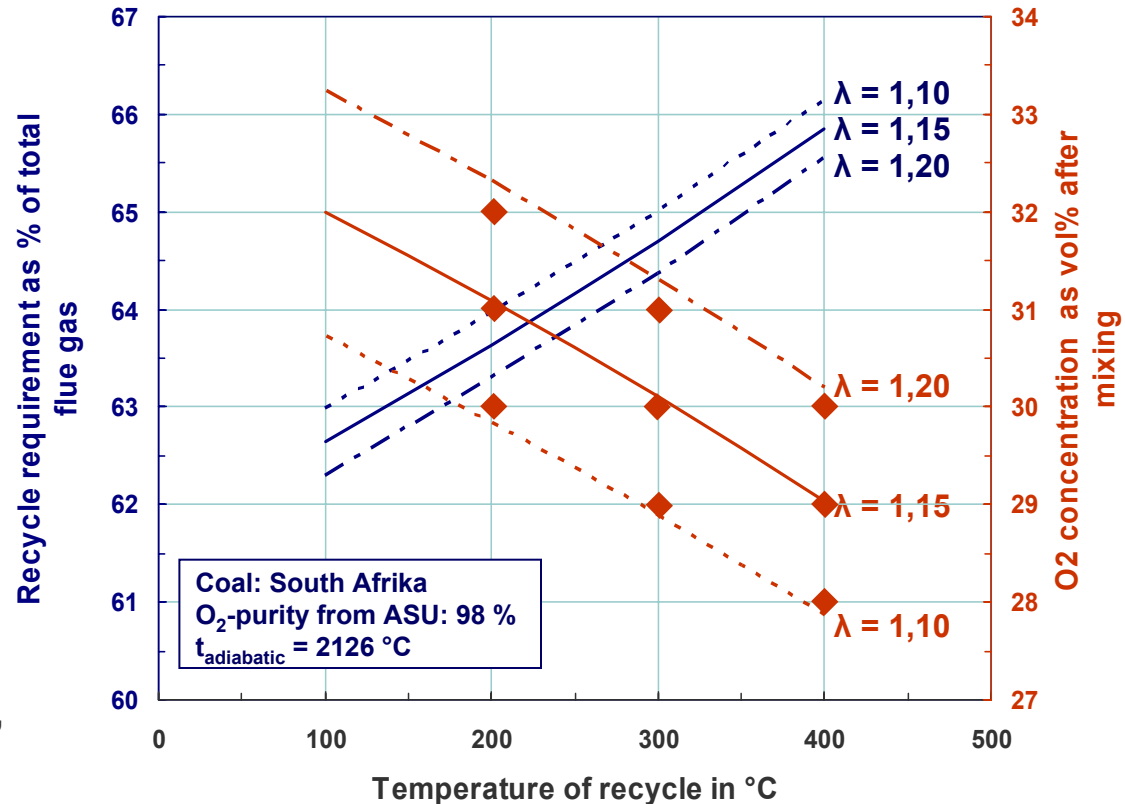
Coal	Composition (in wt%)							NCV MJ/kg	$t_{\text{ad,Air}}$ °C
	C	H	O	S	N	Ash	H <sub>2</sub> O		
South Africa	65,93	3,63	7,25	0,61	1,58	13,60	7,40	25,40	2126
Indonesia	58,70	4,43	8,82	1,00	1,05	5,00	21,0	22,69	2008
Russia	70,09	3,70	7,37	0,30	1,23	9,81	7,50	27,20	2160

- **First approach:** Oxygen and recycled flue gas are mixed completely before combustion
- **Feed-gas composition:** is calculated assuming complete combustion

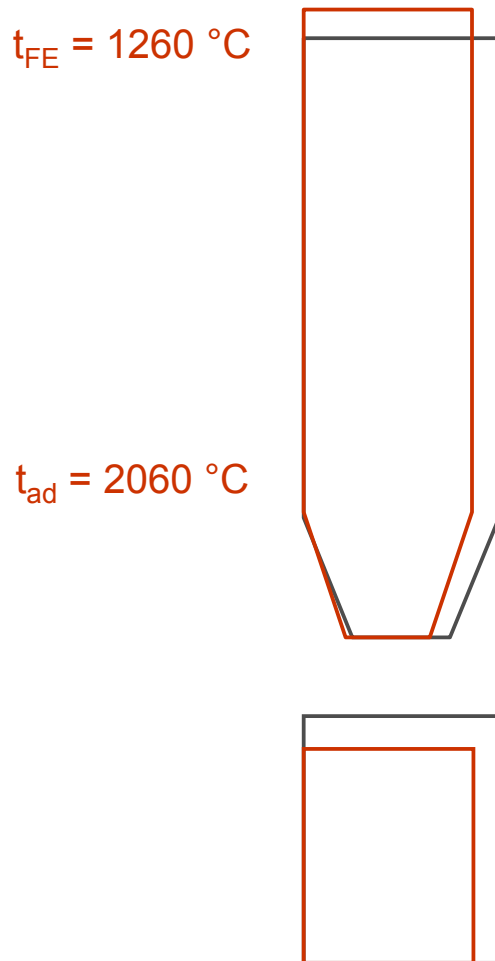
**To reach an equal adiabatic temperature the oxygen concentration**

- rises by reducing the recycle,
- is always above 21 vol%.

- **First combustion experiments (◆)**

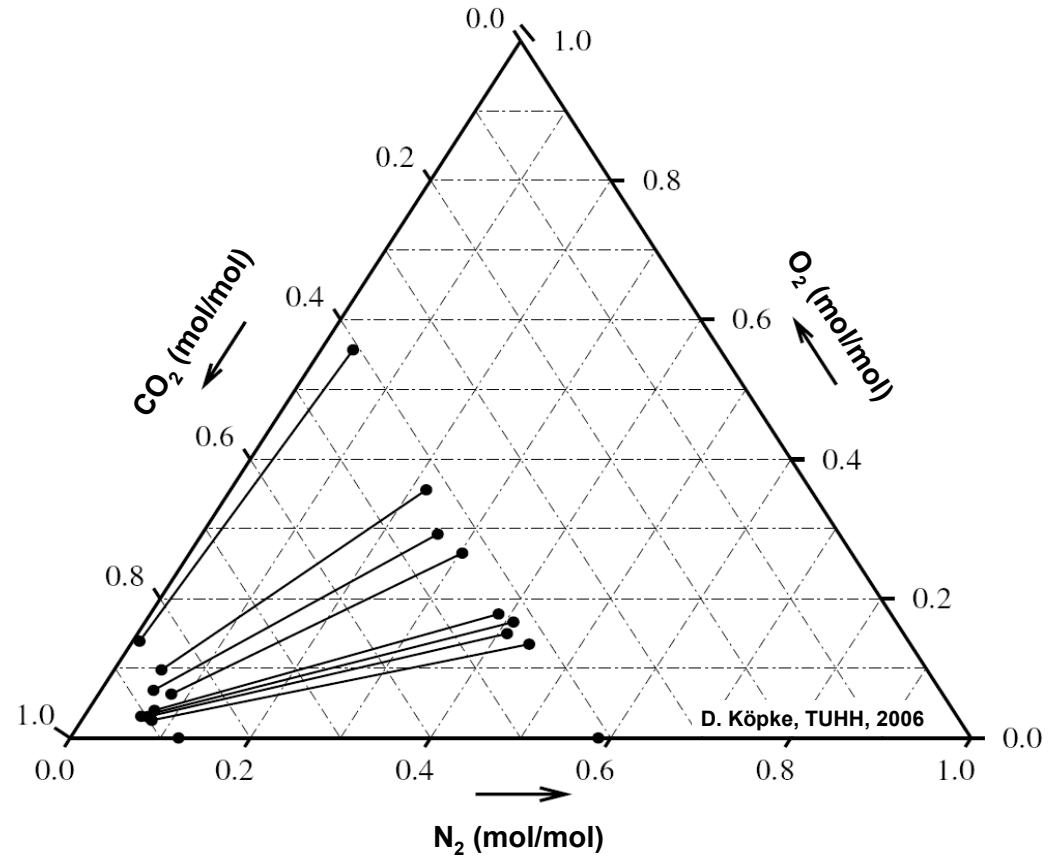
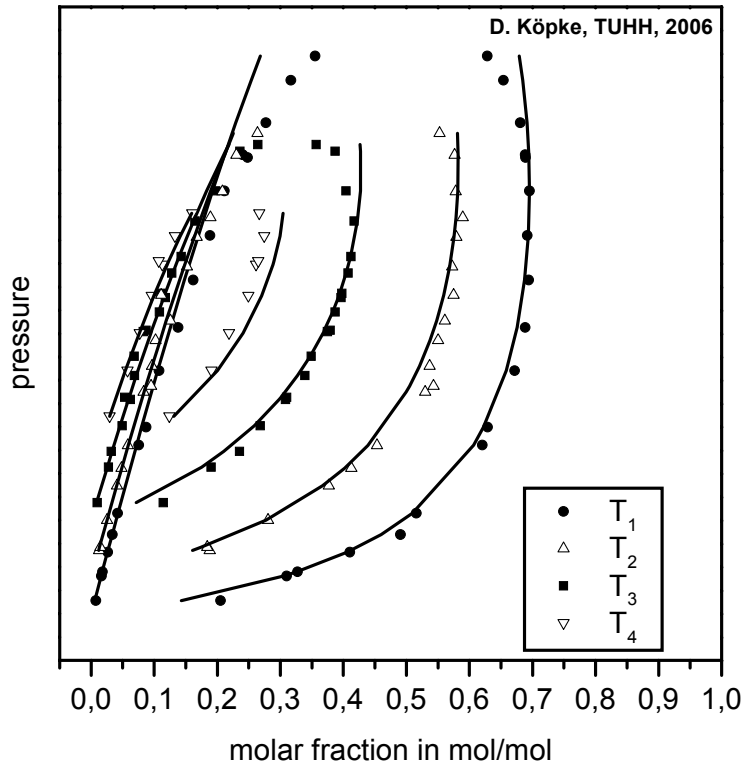


## Comparison of the furnace dimensions of a conventional boiler with an Oxyfuel boiler of equal thermal power

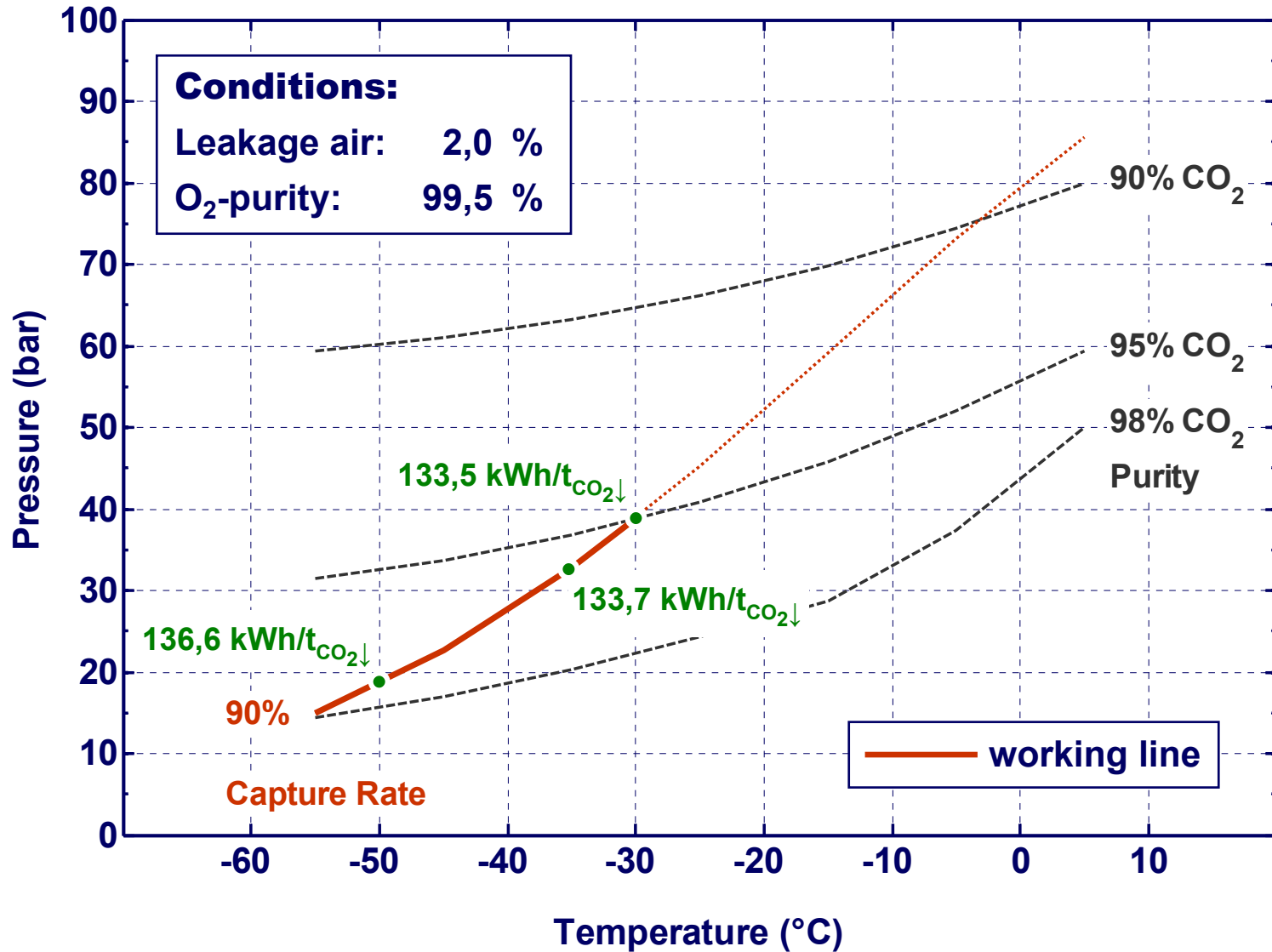


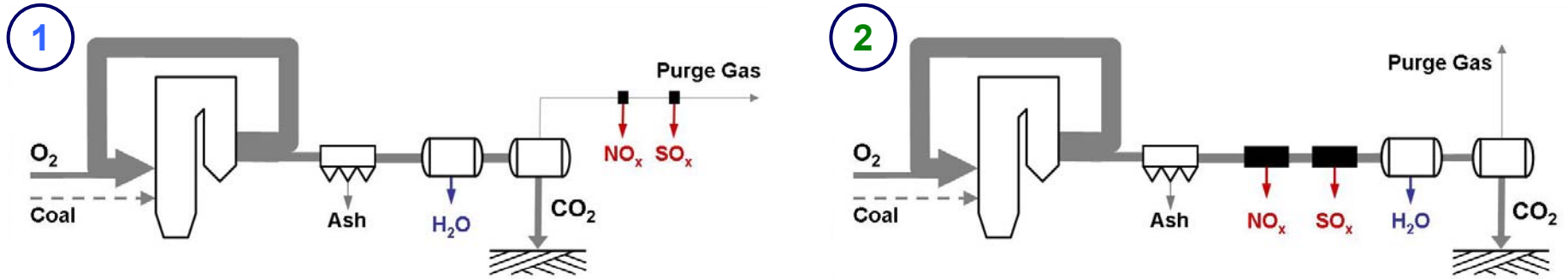
- $\approx 15 \%$  lower flue gas mass stream
- $\approx 22 \%$  higher density of the flue gas
  - ➔  $\approx 30 \%$  smaller cross section of furnace
  - ➔  $\approx 17 \%$  smaller circumference of furnace
  - ➔ furnace  $\approx 17 \%$  higher with unchanged heat transfer
- Improved radiant heat transfer ( $\text{H}_2\text{O}$ ,  $\text{CO}_2$ , dust) leads to  $\approx 5 \%$  higher furnace

- Binary phase equilibria measurements
- Multi component phase equilibria measurement

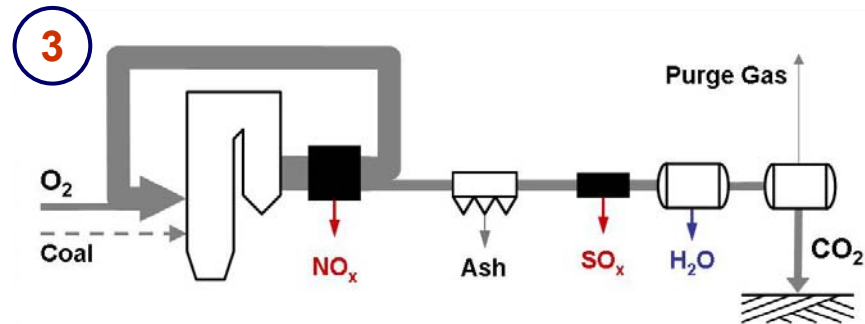


# p-T-diagram for single-stage cryogenic CO<sub>2</sub>-liquefaction





**Basic Conditions:**  
Leakage air: 1.0 %  
O<sub>2</sub>-purity: 99.5 %

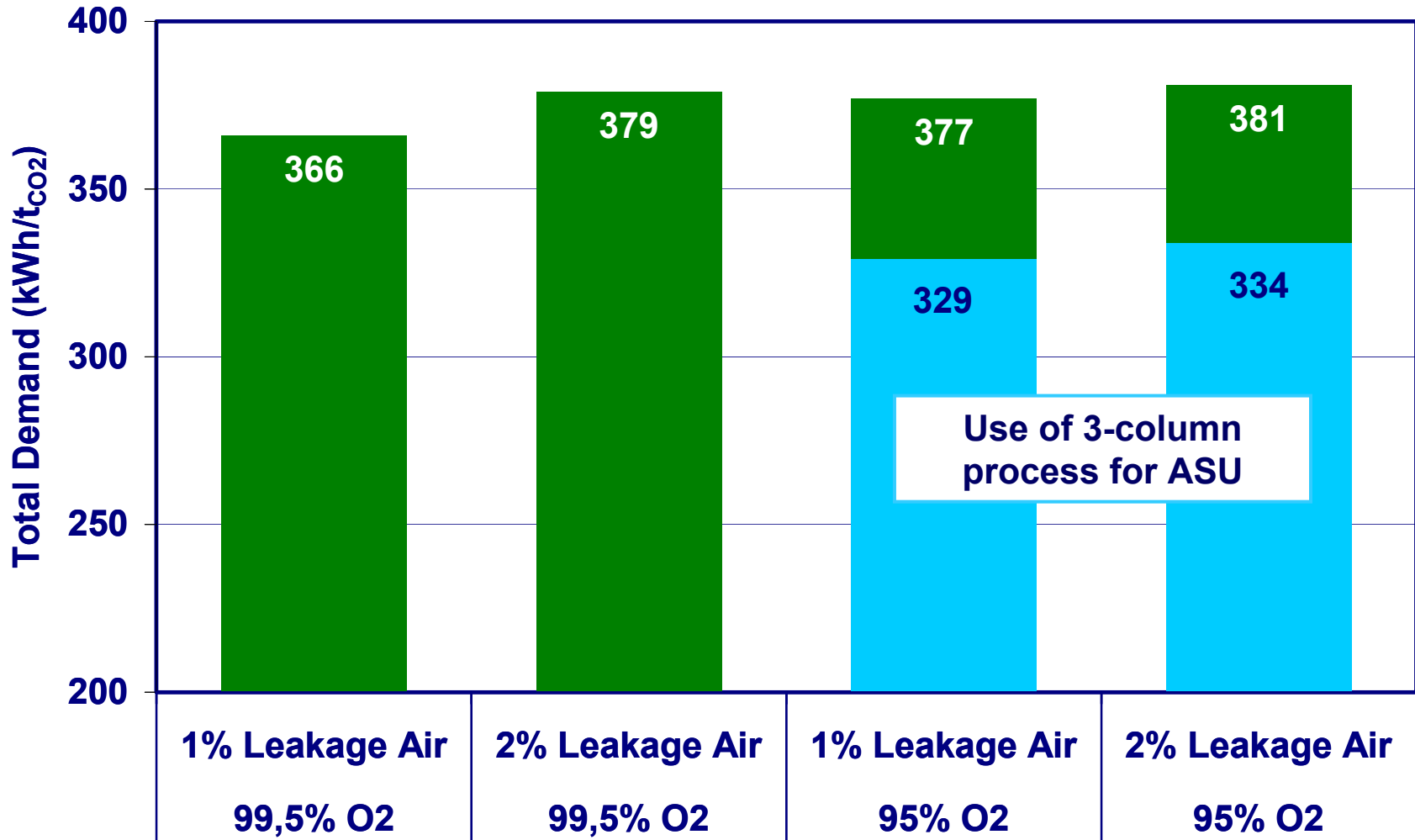


Purity of liquefied CO<sub>2</sub> (in mol-%)

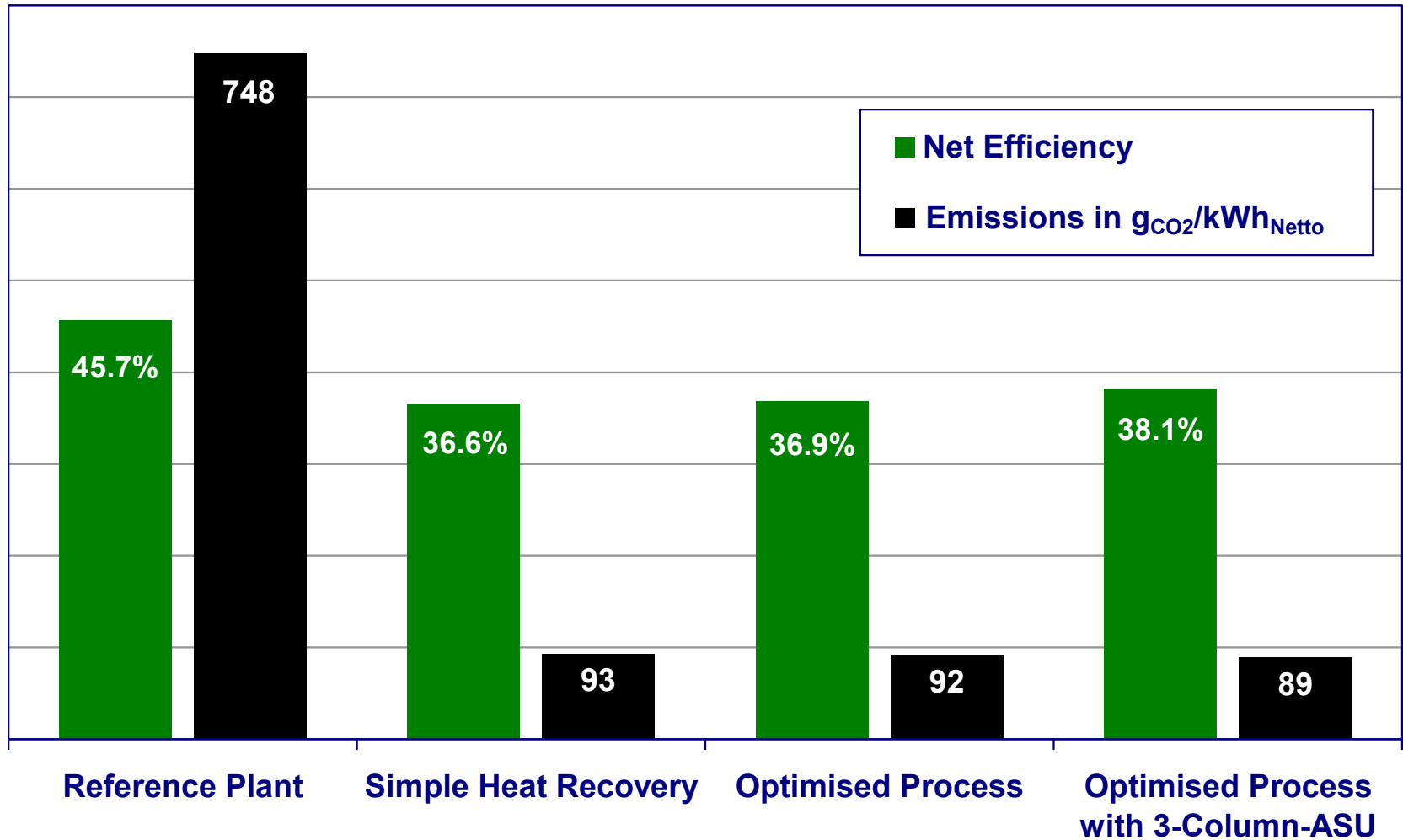
	CO <sub>2</sub>	N <sub>2</sub>	Ar	O <sub>2</sub>	SO <sub>2</sub>	NO <sub>x</sub>
1	98.4	0.6	0.2	≈ 0.4	≈ 0.4	≈ 470 ppm
2	98.8	0.6	0.2	≈ 0.4	≈ 56 ppm	≈ 47 ppm
3	98.8	0.6	0.2	≈ 0.5	≈ 56 ppm	≈ 22 ppm



Requirements: 90 % capture rate and purity > 95%



# Comparison of Different Processes (1% Leakage, Capture Rate 90%, Purity > 98,5%)



- Underlying reference technology

- Reference power plant North-Rhine Westphalia:  $\eta = 45.7\%$  (net)  
power output: 556 MW (net), 600 MW (gross)

- Key power consumers (based on 600 MW gross power output)

- Air Separation Unit:

- $\approx 90$  MW to attain 99.5 vol% oxygen purity

- $\approx 70$  MW at the expense of oxygen purity (95 %) using a new, not yet realized separation technology (3-column-process)

- CO<sub>2</sub> Separation Unit (90 % separation, 1 % leakage air):

- $\approx 47$  MW possibly lower due to optimization

- Estimated efficiency loss:  $\Delta\eta = 8 \dots 10 \dots 11.5\%$  abs.

**Thank You!**